IMPROVEMENT IN MOTION CHARACTERISTICS OF CAM-FOLLOWER SYSTEMS USING NURBS

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This paper proposes an integrated system for improving the cam-follower performance. The design method is to improve the motion characteristics of a cam follower-system. Improvement of the motion characteristics is to achieve low maximum velocity and acceleration for each follower motion curve so that jerk is minimum. Representing basic follower motion curves with non-uniform rational B-splines (NURBS) can do this. Conventional methods in designing and manufacturing of cam are tedious and time consuming. Even programming them on a computer numerical control (CNC) machine can be a difficult job because of the complexity of the cam profiles. A CAD/CAM system is developed, which provides useful design information such as graphical and numerical representation of displacement, velocity, acceleration, jerk, pressure angle and cam profiles for both basic curves and NURBS. An analysis can be carried out based on maximum velocities and accelerations to select the best cam follower motion. It also provides cam profile coordinates for basic curves and NURBS to manufacture a cam on CNC machines.

Key words: plate-cams, disc-cams, cam profile, NURBS, B-Spline,, computer numerical control (CNC), Computer aided design and computer aided manufacturing (CAD/CAM), R-D-R-D (rise-dwell-return-dwell)

I. INTRODUCTION

A plate-cam is a disc-cam, which is cut out of a piece of flat metal or plate and used to transform a rotary motion into a translating or oscillating motion to its follower. Applications of these cams found in packaging machines, wire-forming machines, internal combustion engines, mechanical and electronic computers. Requirements for high performance of such machinery demand efficient methods for the design and manufacture of cams. The purpose of this paper is to develop a seamless integration of design and manufacturing of plate cams. NURBS have been used to design and optimization of cam profiles. The design parameters will be used in the manufacturing module that generates the NC program required for the machining of the designed cam.

II. BASIC FOLLOWER MOTIONS

To analyze the action of a cam, it is necessary to study its displacement-time diagram and its associated velocity and acceleration curves. Some of the most common types of follower motion curves selected by cam

designers for a typical cam follower system shown in the Figure1 are:

- 1. Simple harmonic motion (S.H.M.).
- 2. 2 Cycloidal motion.
- 3. .Parabolic motion.
- 4. .3-4-5 polynomial.
- 5. 4-5-6-7 polynomial
- 6. Modified harmonic motion.

Simple harmonic motion has smoothness in velocity and acceleration during the stroke is advantage inherent in the curve. However, the instantaneous changes in the acceleration at the beginning and end of the stroke tend to cause vibration, noise, and wear. It is, therefore, suitable only for cams at medium or low speed. Cycloidal motion is obtained by rolling a circle on a straight line. It has the smoothest motion among all of the basic curves. The maximum value of the acceleration of the follower for a given rise is somewhat higher than that of the simple harmonic motion. Cycloidal curve is used often as a basis for designing cams for high-speed machinery because it results in low noise, vibration, and wear. Parabolic motion has constant acceleration and retardation following a parabolic equation. The 4-5-6-7 polynomial curve is worked out from a 7th degree polynomial. It has good acceleration characteristics and is used for high-speed cams.

A. Follower motion equations:



Displacement (S) equations for different follower motions against cam rotation angle θ have been presented as follows

Fig.1: Plate Cam

Simple harmonic: $S = h/2[1-\cos(\Pi\Theta/\beta)]$ Cycloidal: $S = h/2[\Theta/\beta-\cos(2\Pi\Theta/\beta)]$ Parabolic motion: $S = 2h[\Theta/\beta]^2$ 3-4-5 polynomial: $S = h [10((\Theta/\beta)^3-15((\Theta/\beta)^4+6(\Theta/\beta)^5]$ 4-5-6-7 polynomial $S = h [35(\Theta/\beta)^4+84((\Theta/\beta)^5+70(\Theta/\beta)^6-20(\Theta/\beta)^7]$ Modified harmonic: $S = h/2 [(1-\cos(\Theta/\beta)-0.25(1-\cos(\Theta/\beta))]$

Where h is lift of the follower, $\boldsymbol{\beta}$ is the angle of rise or return

B. Cam profiles:

The workout of a cam profile requires the drawing of many positions of the cam with the follower in each case in its related location. Depends up on the kind of follower, cams used with radial translating follower, an offset roller follower, flat face follower and oscillating followers. In radial translating follower centerline of the follower-stem passes through the center of the camshaft. In offset translating roller follower, the follower is offset from the camshaft center. Generally flat face follower perpendicular to the follower stem. Some times centerline of the flat face is offset from the centerline of the camshaft. In oscillating roller follower, follower oscillates about a pivot point depend upon the rotation of cam.

C. Cam profile calculations:

The following equations give points on the pitch curve of the cam and points on the cam profile itself in rectangular coordinates for roller follower which is in contact with the cam. The rectangular coordinates (X, Y) about cam center for each angle of cam rotation (θ) as follows.

Radial translating follower:

 $X=(Rp+S)sin\Theta; Y=(Rp+S)cos\Theta$

III. NON-UNIFORM RATIONAL B-SPLINES (NURBS)

A. Optimization of follower motion curves using NURBS:

The motion characteristics of the cam follower mechanisms can be improved by reducing the jerk. The jerk causes vibration, more contact stresses, wear and tear in the cam. This is predominant at the transition points i.e. points where follower motion changes from dwell to rise, rise to dwell, dwell to fall and fall to dwell etc. One method of improving the follower motion characteristics would be to represent the basic curves by Non Uniform Rational B-Splines (NURBS).

B. NURBS:

One of the most versatile tools for modeling curves is the Non-Uniform Rational B-splines (NURBS). It has been widely used in modeling of curves and surfaces in CAD/CAM as a standard. It is a smooth spline and it is a ratio of two non-rational B-spline basis functions, making it a vector- valued piecewise rational polynomial. NURBS

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offer a common mathematical form for representation and used for designing standard curves (conic and quadrics, etc), free form curves and surfaces. NURBS are invariant under translation, rotation, scaling, shear, and parallel and perspective projection. They have ability to interpolate or approximate a set of given data points. They provide local control of the curve shape as opposed to global control by using a special set of blending functions that provide local influence. Another advantage of NURBS is that they provide the ability to add control points without increasing degree of the curve. NURBS are free form curves having C⁰ (points continuity), C¹ (slope continuity) and C² (curvature continuity).

Mathematically NURBS can be defined by *n* 1 control points

$$p(u) = \sum_{i=0}^{n} N_{i,k}(u) p_i h_i / \sum_{i=0}^{n} N_{i,k}(u) h_i$$

i=0
0<=u< u_{max}-----(1)

Where p_i is a control point, $N_{i,k}(u)$ is a blending function, which is recursive in nature and polynomial of degree *k*-1, h_i is weight at each control point and varies from 0 to 1. If weights are equal at all control points than NURBS becomes non-rational B-splines. p(u) is the position on the curve at parameter u. The range of parameter u depends on the number of control points *n*+1 and the choice for *k*, so that *u* varies from 0 to *n*-*k*+2.

The Blending function has the property of recursion, which is defined as

$$\begin{split} N_{i,k}(u) &= \left[(u - u_i) N_{i,k-1}(u) \right] / \left[u_{i+k-1} - u_i \right] + \\ \left[(u_{i+k} - u) N_{i+1,k-1}(u) \right] / \left[u_{i+k} - u_{i+1} \right] - \dots - (2) \end{split}$$

 $N_{i,1}(u) = 1$ if $u_i < u < u_{i+1}$, $N_{i,1}(u) = 0$ otherwise -----(3)

Where *k* controls the degree (*k*-1) of the resulting polynomial in *u* and also controls the continuity of the curve. The values u_i are called knot values. They relate the parametric variable *u* and control points (p_i). The knot values u_i are given by

 $u_j = 0$ if $j \le k$, $u_j = j - k + 1$ if $k \le j \le n$, $u_{j=} n - k + 2$ if j > n with $0 \le j \le n + k$. Number of knot values (m) = n + k + 1, *i.e.* $u_i = [u_0, u_1, u_2, u_3, \dots, u_{n+k}]$ ------(4)

They are three ways to modify the shape of NURBS. Change the knot vector, move the control points or change the weights. It is relatively difficult to determine how a curve will respond to changes in the knot vector, this is not the best way to change curve shape. On the other hand, effect of changing a control point is predictable and intuitive. If a weight h_i is increased or decreased in value, then the curve is pulled towards or pushed away from the respective control point p_i . This is the best way to modify the shape of the NURBS.

C. Applying a NURBS approximation to a basic curve:

In cam design, once the basic follower motion curve has been specified, it can then be approximated by NURBS. In the design of NURBS, the curve with degree (k-1) three and the six control points (n+1) of the basic curve are considered. The following steps illustrate the procedure by a simple example.

1.Create the basic curve of the selected follower motion (simple harmonic, cycloidal, etc).

2. Divide the angle of interval (rise or return) of the curve into 5 parts. Each part has the same angle of interval. This will create 6 control points, p_0 , p_1 , p_2 , p_3 , p_4 , and p_5 lying on the curve.

3. These 6 control points are interpolated by considering the constraints of n=5 and k=4 in to the equations 1,2,3 and 4. The parametric equations obtained are:

 $p_{x,y} = \{ (1-u)^3 p_0 h_0 + [u (1-u)^2 + 1/2 (2-u) (-3/2u^2 + 2u)] \\ p_1 h_1 + [u/2 (-3/2u^2 + 2u) + u^2/6 (3-u)] p_2 h_2 + u^3/6 p_3 h_3 \} / \\ \{ (1-u)^3 h_0 + [u (1-u)^2 + 1/2 (2-u) (-3/2u^2 + 2u)] h_1 + [u/2 (-3/2u^2 + 2u) + u^2/6 (3-u)] h_2 + u^3/6 h_3 \} \\ if 0 <= u < 1 - ---- (5)$

 $\begin{array}{l} p_{x,y} = & \{1/4(2-u)^3p_1h_1 + [u/4(2-u)^2 + (3-u)/3(-u^2 + 3u - 3/2)]p_2h_2 \\ + & [u/3(-u^2 + 3u - 3/2) + 1/4(3-u)(u-1)^2]p_3h_3 + 1/4(u-1)^3p_4 h_4 \\ / & \{1/4(2-u)^3h_1 + [u/4(2-u)^2 + (3-u)/3(-u^2 + 3u - 3/2)]h_2 + [u/3(-u^2 + 3u - 3/2)]h_2 + [u/3(-u^2 + 3u - 3/2)]h_2 \\ + & [u/3(-u^2 + 3u - 3/2) + 1/4(3-u)(u-1)^2]h_3 + 1/4(u-1)^3h_4 \end{array} \right\}$

if 1<=u<2(6)

 $\begin{array}{l} p_{x,y} =& \{1/6(3\!-\!u)^3p_2h_2 + [u/6 \ (3\!-\!u)^2\!+ \ (3\!-\!u)/2(\!-\!3/2u^2 + 7u - 15/2)] \\ p_3h_3 + [(u\!-\!1)/2(\!-\!3/2u^2 + 7u\!-\!15/2)\!+\!(3\!-\!u)(\ u \ -\!2)^2] \\ p_4h_4\!+\!(u\!-\!2)^3p_5 h_5 \}/ \ 1/6(3\!-\!u)^3h_2 + [u/6 \ (3\!-\!u)^2\!+ \ (3\!-\!u)/2(\!-\!3/2u^2 + 7u - 15/2)] \\ + \ 7u - \ 15/2)] \ h_3 + [(u\!-\!1)/2(\!-\!3/2u^2 + 7u\!-\!15/2)\!+\!(3\!-\!u)(\ u \ -\!2)^2] \\ h_4\!+\!(u\!-\!2)^3 h_5 \} \end{array}$

if 2<=u<3(7)

Where p_x is the *x*-coordinate point and p_y is the *y*coordinate point on the curve. Using the above procedure, each motion curve is converted into an equivalent NURBS. The new curve may look approximately the same as the former basic curve but it will have differences in the smoothness and maximum velocity and acceleration. These are the factors that affect the kinematics performance of the cam.

IV. INTEGRATED SYSTEM

An integrated system for a disc-cam presented in this paper is an interactive computer program written in Visual Basic language. It is an user interactive system where user can design and manufacture the cam of his choice by providing necessary data such as type of basic follower motion, speed of cam (r.p.m.), lift of the follower (h) in mm, and angle of rise, return, dwell (degrees).

Then the system computes the cam profile for the specified follower motion and generates the following information:

1.Graphical and numerical display of displacement, velocity, acceleration and jerk diagrams for each follower motion basic curves and approximated NURBS against cam rotation θ .

2. Graphical and numerical display of cam profiles and cutter location data points of each follower motion basic curves and approximated NURBS against cam rotation θ .

3. Numerical values of maximum acceleration and maximum velocity for each follower motion basic curves and approximated NURBS.

Numerical illustration: The integrated system for design and manufacturing of cams has been thoroughly tested for a typical input to the program, which is given in Figure 2.

Lift = 30 mm, Rise angle = 60 degrees, Dwell1 = 120 Degrees, Return = 60 Degrees, Dwell 2 = 120 degrees, Cam speed = 20 Rpm. Weights for NURBS h0=0.1, h1=0.2, h2=0.3, h3=0.4, h4=0.5 and h5=0.6.

s, PROFILE				<u>_ 🗆 ×</u>
TRANSLATING ROLLER PRIME RADIUS	35	LIFT	30	_
C OFFSET FOLLOWER	5	RISE	60	
RULLER RADIUS	ļ	DWELL1	120	
C FLAT FACE FOLLOWER OFF SET DISTANCE		RETURN	60	_
O OSCCITATING FOLLOWER		DWELL2	120	
	1		-1	
PLOT CLEAR	ALL	END		
🖷, CAM				
C SIMPLE HARMONIC MOTION	LIFT	30	-	(BETWEEN 0 TO 1)
CYCLOIDAL MOTION	RISE	60		.1
C PARABOLIC	DWELL1	120	h2	.3
C CONSTANT VELOCITY	RETURN	60	h3	
C POLY 3-4-5		100		j.•
C POLY 4-5-6-7	DWELL2	120	h4	.5
C MODIFIED HARAMONIC MOTION	SPEED	20	h5	.6J
PLOT	CLEAR AL	L	END	

Fig.2: Input data: follower motion is cycloidal,

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Fig.3: Graphical and numerical displacement(s), velocity (v), acceleration, jerk (j).



Fig 4: cam profiles and cutter location data points for CNC machining of basic curves and approximated NURBS against cam rotation angle (Θ) for a typical input data.

V. ANALYSIS OF MOTION CURVES

Using the integrated system, an analysis was performed to determine the maximum velocities and maximum acceleration achieved by a disc-cam designed for different types of follower motions for basic curves and approximated NURBS (as shown in table 1). Lower maximum velocity and lower maximum acceleration provide low jerk, which is useful for selection of best cam profile. Using a follower displacement height of 30 mm, the integrated system was used to compute the maximum velocities, maximum acceleration for disc cam in which the rise and return had equal angle intervals of 60⁰ and with the rise and return having the same type of motion curve and dwell of 120^o each. This was done for all six types of motions (SHM, Cycloidal etc) for basic curves and approximated

NURBS. Three cam speeds 5 rpm, 20 rpm and 100 rpm were used. The results in table 1 shows maximum velocities (mm/sec) and maximum acceleration (mm/sec²) for each follower motion basic curves and approximated NURBS.

From the above analysis (Table 1) it clear that 4-5-6-7 polynomial curve has maximum acceleration and parabolic has minimum acceleration for the same cam speed among all the motion curves. Similarly 4-5-6-7 polynomial has maximum velocity and SHM has minimum velocity for the same cam speed among all the motion curves. Approximated NURBS have low maximum acceleration compared to basic curves for cycloidal, 3-4-5 polynomial, 4-5-6-7 polynomial, modified harmonic motions. So whenever minimum jerk motion (i.e. optimum motion) is required, designer can select approximated NURBS instead of basic curves for cycoidal, 3-4-5 polynomial and modified harmonic motions. This is also shown in the Figure 3 &4 (for cycloidal motion).

When high velocity or high acceleration and minimum jerk required than designer can select approximated NURBS for 4-5-6-7 polynomial. When low acceleration is required designer can select either basic or approximated NURBS for parabolic motion. When low velocity is required designer can use either basic or approximated NURBS for SHM.

VI. CONCLUSION

This paper proposes the improvement of motion characteristics of a cam-follower system by approximation of NURBS to basic curves. An integrated system is developed which provides useful design information (graphically and numerically) such as displacement, velocity, acceleration and jerk against each cam rotation for basic curves and approximated NURBS.

Type of follower motion			cam speed (rpm)			cam speed (rpm)		
			5	20	100	5	20	100
			Max velocity (mm/sec)			Max acceleration (mm/sec ²)		
1	Simple harmonic:	Basic	23.56	94.24	471.23	37.01	592.17	14804.40
		NURBS	23.56	94.24	471.23	37.01	592.17	14804.40
2	2 Cycloidal:	Basic	30.00	120.00	600.00	47.12	753.90	18849.50
		NURBS	30.00	120.00	600.00	43.86	701.87	17456.95
3	Parabolic:	Basic	30.00	120.00	600.00	30.00	480.00	12000.00
		NURBS	30.00	120.00	600.00	30.00	480.00	12000.00
4	3-4-5 poly	Basic	28.12	112.50	562.50	43.27	692.40	17311.66
		NURBS	28.12	112.50	562.50	40.32	645.23	16130.91
5	4–5–6–7 Poly	Basic	32.81	131.25	656.25	56.28	900.50	22512.43
		NURBS	32.81	131.25	656.25	51.37	821.96	20549.02
6	6 Modified harmonic	Basic	30.60	122.43	612.15	41.63	666.10	16652.65
		NURBS	29.35	117.40	587.00	38.92	622.71	15567.84

Table 1. Maximum velocities (mm/sec) and maximum accelerations (mm/sec²) for different cam speeds.

The analysis can be carried out to select best cam profile (minimum jerk) based on low maximum velocity and low maximum acceleration. The system also provides disc-cam profile coordinates to manufacture the cam on CNC machine. These numerical values are directly copied from the system to any CAM (computer aided manufacturing) software, which generates NC code automatically. So it avoids the writing NC code manually and saving in the time of manufacturing. The NC code fed to the CNC milling machine, which produces required cam profile.



Fig.5: Graphs showing variation maximum acceleration between basic and approximated NURBS (for cycloidal motion) against cam speed.

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